## § 178.338-5

- (d) Substructures must be properly fitted before attachment and the welding sequence must minimize stresses due to shrinkage of welds.
- (e) Filler material containing more than 0.05 percent vanadium may not be used with quenched and tempered steel.
- (f) All tank nozzle-to-shell and nozzle-to-head welds must be full penetration welds.

(Approved by the Office of Management and Budget under control number 2137–0017)

[Amdt. 178-77, 48 FR 27704 and 27713, June 16, 1983, as amended at 49 FR 24316, June 12, 1984]

#### § 178.338-5 Stiffening rings.

- (a) A tank is not required to be provided with stiffening rings, except as prescribed in the ASME Code.
- (b) If a jacket is evacuated, it must be constructed in compliance with §178.338-1(f). Stiffening rings may be used to meet these requirements.

[Amdt. 178–77, 48 FR 27704, June 16, 1983]

# § 178.338-6 Manholes.

- (a) Each tank in oxygen service must be provided with a manhole as prescribed in the ASME Code.
- (b) Each tank having a manhole must be provided with a means of entrance and exit through the jacket, or the jacket must be marked to indicate the manway location on the tank.
- (c) A manhole with a bolted closure may not be located on the front head of the tank.

[Amdt. 178–77, 48 FR 27704, June 16, 1983, as amended at 49 FR 24316, June 12, 1984]

# §178.338-7 Openings.

- (a) The inlet to the liquid product discharge opening of each tank intended for flammable ladings must be at the bottom centerline of the tank.
- (b) If the leakage of a single valve, except a pressure relief valve, pressure control valve, full trycock or gas phase manual vent valve, would permit loss of flammable material, an additional closure that is leak tight at the tank design pressure must be provided outboard of such valve.

[Amdt. 178-77, 48 FR 27704, June 16, 1983]

# § 178.338-8 Pressure relief devices, piping, valves, and fittings.

- (a) Pressure relief devices. Each tank pressure relief device must be designed, constructed, and marked in accordance with §173.318(b) of this subchapter.
- (b) Piping, valves, and fittings. (1) The burst pressure of all piping, pipe fittings, hoses and other pressure parts, except for pump seals and pressure relief devices, must be at least 4 times the design pressure of the tank. Additionally, the burst pressure may not be less than 4 times any higher pressure to which each pipe, pipe fitting, hose or other pressure part may be subjected to in service.
- (2) Pipe joints must be threaded, welded or flanged. If threaded pipe is used, the pipe and fittings must be Schedule 80 weight or heavier. Malleable metals must be used in the construction of valves and fittings. Where copper tubing is permitted, joints shall be brazed or be of equally strong metal union type. The melting point of the brazing materials may not be lower than 1000 °F. The method of joining tubing may not reduce the strength of the tubing, such as by the cutting of threads
- (3) Each hose coupling must be designed for a pressure of at least 120 percent of the hose design pressure and so that there will be no leakage when connected.
- (4) Piping must be protected from damage due to thermal expansion and contraction, jarring, and vibration. Slip joints are not authorized for this purpose.
- (5) All piping, valves and fittings on a cargo tank must be proved free from leaks. This requirement is met when such piping, valves, and fittings have been tested after installation with gas or air and proved leak tight at not less than the design pressure marked on the cargo tank. This requirement is applicable to all hoses used in a cargo tank, except that hose may be tested before or after installation on the tank.
- (6) Each valve must be suitable for the tank design pressure at the tank design service temperature.
- (7) All fittings must be rated for the maximum tank pressure and suitable for the coldest temperature to which

they will be subjected in actual service.

- (8) All piping, valves, and fittings must be grouped in the smallest practicable space and protected from damage as required by §178.338-10.
- (9) When a pressure-building coil is used on a tank designed to handle oxygen or flammable ladings, the vapor connection to that coil must be provided with a valve or check valve as close to the tank shell as practicable to prevent the loss of vapor from the tank in case of damage to the coil. The liquid connection to that coil must also be provided with a valve.

[Amdt. 178–77, 48 FR 27704, June 16, 1983, as amended by Amdt. 178–89, 54 FR 25019, June 12, 1989]

## §178.338-9 Holding time.

- (a) "Holding time" is the time, as determined by testing, that will elapse from loading until the pressure of the contents, under equilibrium conditions, reaches the level of the lowest pressure control valve or pressure relief valve setting.
- (b) Holding time test. (1) The test to determine holding time must be performed by charging the tank with a cryogenic liquid having a boiling point, at a pressure of one atmosphere, absolute, no lower than the design service temperature of the tank. The tank must be charged to its maximum permitted filling density with that liquid and stabilized to the lowest practical pressure, which must be equal to or loading. The cargo tank together with its contents must then be exposed to ambient temperature.
- (2) The tank pressure and ambient temperature must be recorded at 3hour intervals until the pressure level of the contents reaches the set-to-discharge pressure of the pressure control valve or pressure relief valve with the lowest setting. This total time lapse in hours represents the measured holding time at the actual average ambient temperature. This measured holding time for the test cryogenic liquid must be adjusted to an equivalent holding time for each cryogenic liquid that is to be identified on or adjacent to the specification plate, at an average ambient temperature of 85 °F. This is the

rated holding time (RHT). The marked rated holding time (MRHT) displayed on or adjacent to the specification plate (see §178.338–18(b)(9)) may not exceed this RHT.

- (c) Optional test regimen. (1) If more than one cargo tank is made to the same design, only one cargo tank must be subjected to the full holding time test at the time of manufacture. However, each subsequent cargo tank made to the same design must be performance tested during its first trip. The holding time determined in this test may not be less than 90 percent of the marked rated holding time. This test must be performed in accordance with §§ 173.318(g)(3) and 177.840(h) of this subchapter, regardless of the classification of the cryogenic liquid.
- (2) Same design. The term "same design" as used in this section means cargo tanks made to the same design type. See §178.320(a)(3) for definition of "design type".
- (3) For a cargo tank used in nonflammable cryogenic liquid service, in place of the holding time tests prescribed in paragraph (b) of this section, the marked rated holding time (MRHT) may be determined as follows:
- (i) While the cargo tank is stationary, the heat transfer rate must be determined by measuring the normal evaporation rate (NER) of the test cryogenic liquid (preferably the lading, where feasible) maintained at approximately one atmosphere. The calculated heat transfer rate must be determined from:

$$q = [n(\Delta h)(85-t_1)] / [t_s - t_f]$$

Where

- q = calculated heat transfer rate to cargo tank with lading, Btu/hr.
- n = normal evaporation rate (NER), which is the rate of evaporation, determined by the test of a test cryogenic liquid in a cargo tank maintained at a pressure of approximately one atmosphere, absolute, lb/hr.
- $\Delta$  h = latent heat of vaporization of test fluid at test pressure, Btu/lb.
- at test pressure, Bullo.  $t_s$  = average temperature of outer shell during test, °F.
- t<sub>1</sub> = equilibrium temperature of lading at maximum loading pressure, °F.
- $t_f$  = equilibrium temperature of test fluid at one atmosphere,  ${}^{\circ}F$ .
- (ii) The rated holding time (RHT) must be calculated as follows: